

IN-VITRO COMPARATIVE STUDY OF COMPRESSIVE STRENGTH IN CAD/CAM DENTAL MATERIALS

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ABSTRACT

Aim of the study was to investigate comparatively the compressive strength for three computer-aided design/computer-aided manufacturing (CAD/CAM) dental materials: glass ceramic IPS Empress CAD (Ivoclar Vivadent), hybrid ceramic Cerasmart (GC) and polymer-reinforced graphene G-CAM (Graphenano Dental). **Material and methods** 45 samples consisted of the single-unit molar crowns fabricated by three CAD/CAM materials were cemented adhesively on 3D printed abutments (Asiga Dental Resin). The samples were divided into 3 groups (n=15) according to the crowns thickness; group 1 under the cusps/cervical margins - 0.6 mm/0.4 mm, group 2 - 1 mm/0.7 mm respectively, and group 3 - 1.5 mm/1 mm. Additionally, 20 cylindrical specimens fabricated by the three crowns and abutments material (n=5) were prepared by CAD/CAM technique. All samples and specimens were subjected to an axial compressive load by using a universal testing machine (Instron 3366-10kN, USA) until fracture. **Results** The compressive strength values were 1258 MPa for Empress CAD, 501.3 MPa for Cerasmart, 435 MPa for G-CAM and 360 MPa Asiga resin. G-CAM crowns exhibited a higher maximum compressive load (1701.5-2011.8N) than both Cerasmart (1295.4-1642.9N) and Empress CAD (494.3-597.5N). **Conclusions** The CAD/CAM crown materials presented different mechanical behavior; Empress CAD and Cerasmart presented a fragile behavior, with a high compressive strength when compared to G-CAM and Asiga resins.

Key words: CAD/CAM, nanoceramic resin, graphene-reinforced polymer, compressive strength

INTRODUCTION

Over the last years, there has been an increased interest in the development of new materials that restore the morphology and functions of tooth loss [1]. These meet the growing demand for the high aesthetics, biocompatibility, and long-term longevity of prosthetic restorations [2]. Conventional techniques used for fabrication of dental prosthesis are being replaced with

computer aided design/computer aided manufacturing (CAD/CAM) technology, as it provides a series of advantages, such as shorter prosthetic treatment time by using digital impressions and models, virtual articulators, and specific materials [2-5].

With the evolution of digital technology through the precise milling of CAD/CAM materials, the mechanical

characteristics of definitive restorations are improved [6]. At present, several such materials are available to be processed through CAD/CAM technology, like glass ceramics, composite resins [7-9] and graphene-reinforced polymers [10].

CAD/CAM glass-ceramics are composed of glass and crystal phases. The glass phase gives their aesthetic aspect and translucency, while the crystal phase influences the mechanical properties of the materials; the ratio between the two phases determines the characteristics of the final restoration [11,12]. IPS Empress® CAD (Ivoclar Vivadent) is a leucite-reinforced glass ceramic which contains 35-45% leucite crystals with a particle size between 1 and 5 microns, embedded in a glassy matrix [13,14]. Given the increased concentration of the crystals, mechanical parameters such as the fracture strength calculated at 180 MPa limit the use of leucite-based ceramics to single tooth restorations, including inlays, onlays and crowns in the posterior region, where the masticatory forces are higher [11,13,14].

A study conducted by Brochu&El-Mowafy showed a survival rate of IPS Empress crowns after 3 to 3.5 years of about 92%-99%, while crown fracture was found to be the main reason for failure [15], followed by supporting teeth fracture because of occlusal stress and insufficient ceramic thickness [16], appearing when the opposing teeth were either natural teeth or ceramic restorations [17]. A review on the clinical fracture rate of crowns fabricated with leucite reinforced ceramic IPS Empress reported that adhesively luted IPS Empress crowns presented a higher fracture rate for molars than for incisors, therefore the authors concluded that these crowns

should have sufficient thickness and are not to be used in patients with bruxism [18].

Cerasmart (GC, Tokyo, Japan) is a CAD/CAM hybrid ceramic composed of a polymer part (29 wt%): 2,2-Bis (4-methacryloxypolyethoxyphenyl) propane (bis-MEPP), urethane dimethacrylate (UDMA), dimethacrylate (DMA), and an inorganic (71wt%): silica SiO₂ (20 nm) and barium glass (300 nm) nanoparticles [7,11]. It combines the positive characteristics of glass ceramics with those of composite resins [19].

A recent study reported that CAD/CAM resin ceramic materials exhibit comparable hardness and elastic modulus to dentine and these mechanical characteristics were correlated to ceramic filler percentage and microstructure [20]. Another study conducted by Sorrentino comparing resistance to fracture and failure mode of Cerasmart (GC, Tokyo, Japan) crowns prepared by CAD/CAM technology with different occlusal thickness, showed that the strength of the samples increased with occlusal thickness. The thickness highly affected the mode of failure but did not influence the fracture resistance of the restoration [21].

A recent type of CAD/CAM material is G-CAM (Graphenano Dental, Spain) launched on the dental market in 2019. It is composed of polymethyl-methacrylate (PMMA), one of the most common materials, first introduced 84 years ago [22] and graphene, first characterized in 2004 [23]. PMMA is a light, aesthetic, and inexpensive polymer, chemically stable but with reduced mechanical resistance that needs reinforcement. Its resistance can be increased by using a variety of reinforcing agents such as fibers, fillers, nanofillers and

rubberlike substances [24,25] such as graphene.

Graphene-based materials can have different applications in dental fields, such as the fabrication of CAD/CAM restorations [10,26]. In a recent study, the elastic modulus and flexural strength of PMMA reinforced with graphene were analyzed and it was found that the graphene determines higher values of its mechanical properties.

The aim of the study is to comparatively investigate the compression properties of a conventional ceramic, IPS Empress (Ivoclar Vivadent, Lichtenstein), a hybrid nanoceramic, Cerasmart (GC, Tokyo, Japan), and a newly marketed graphene-based polymer, G-CAM (Graphenano Dental, Spain), as well as to compare the compressive strength of each crown at different occlusal thicknesses.

MATERIAL AND METHODS

Sample fabrication

Forty-five samples representing the first mandibular molar (abutments and crowns) were digitally designed and fabricated. The abutments were milled out of Asiga Denta Model (Asiga, Australia) 3D printable resin material. The crowns were made from three different CAD/CAM materials: leucite-reinforced glass ceramic IPS Empress CAD (Ivoclar Vivadent, Lichtenstein), hybrid nanoceramic Cerasmart (GC, Tokyo, Japan), and graphene-reinforced polymer G-CAM (Graphenano Dental, Spain). The Empress crowns were wet-milled, the Cerasmart and G-CAM crowns were dry-milled, using the Coritec 150i Pro (Imes-Icore, Germany) 5-axis milling machine. They were divided

into three groups of 15 samples based on the thickness of the material crowns (Table 1).

Table 1. Crown thickness according to the groups

Thickness crowns	Group 1	Group 2	Group 3
Under the cusps	0.6 mm	1 mm	1.5 mm
Cervical margins	0.4 mm	0.7 mm	1 mm

Cementation procedure

The adhesive technique was used for the cementation of the crowns to the corresponding abutments. The internal surfaces of the Empress crowns were treated with 4.6% hydrofluoric acid (IPS Ceramic Etching gel – Ivoclar Vivadent, Schaan, Lichtenstein) for 60 s. For the Cerasmart and G-CAM crowns, the internal surfaces were lightly sandblasted with aluminium-oxide 20 µm particles at 0.2 MPa pressure for 10 s. Then, the primer G-Multi Primer (GC Australasia Dental, Australia) was applied according to the recommendations of manufacturers. For the abutment substrates, the bonding agent G-Premio Bond (GC Australasia Dental, Australia) was applied and cured, using a light-emitting diode curing unit (Zenolite LED Curing Light, President Dental, Germany) with a mean light intensity of 1200 mW/cm². Dual-cure resin cement G-CEM LinkForce™ (GC Australasia Dental, Australia) was added into all crowns and immediately seated onto the abutments. The cement was light cured with 1200 mW LED light-curing unit. After a light prepolymerization of 1-2 s, the

excess of cement was removed, and the final polymerization was applied for 40 s on each surface. After cementation, all samples and specimens were stored in distilled water for one week at room temperature before testing, to ensure the water uptake by the organic phase is completed and mimicking the working conditions from the oral environment.

Specimen fabrication

Twenty cylindrical specimens were prepared from each crowns group and Asiga resin abutment materials with circular cross-section of 4 mm diameter and an anvil height of 8 mm (n=5 per material) used for manufacturing of above-described abutments and crowns. They were polished and finished.

Mechanical testing

Firstly, the cylindrical specimens made of the studied materials were tested under compression, and the mechanical properties evaluated were compressive stress and strain at maximum load and the value of the modulus of elasticity (Young's modulus). Secondly, the molar crowns were tested for the same parameters in the static conditions (Fig.1 a, b).

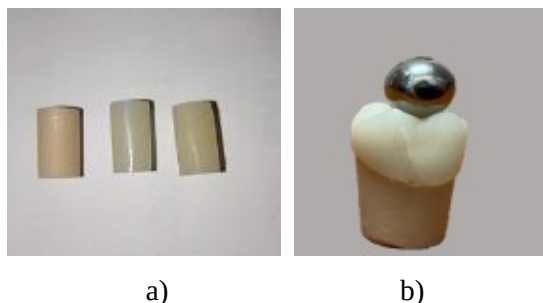


Figure 1. Prepared specimens a) and samples b) for compressive strength testing

– 10kN, Instron, USA) and a uniaxial force was applied vertically from the occlusal surface with a crosshead speed of 1 mm /min along the longitudinal axis of the crowns until fracture. An 8 mm stainless-steel bearing ball was used for the molar crowns to simulate the ideal tripodal contact point of the opposing cusp in the central fossa of the first mandibular molar. The maximum compressive load (N) and compressive extension at maximum load (mm) were recorded by the machine software (Blue Hill, Instron, USA) during the mechanical testing.

Statistical analysis

The data was exported in CSV files and was then aggregated in an Excel worksheet. For the compressive samples and specimens, a mean value and standard deviations were calculated. The results obtained for molar samples were subjected to a more complex statistical analysis using the SPSS v26 software package. To test the difference between material groups, an analysis of variance would be appropriate. Considering the small sample and some violations of the assumptions of the ANOVA test, a non-parametric alternative was used. The Kruskal-Wallis test is a non-parametric alternative, which does not assume that the data comes from a distribution that can be described through parameters such as mean and standard deviation, like in the case of the normal distribution [27]. Like ANOVA it is used when there are three or more groups, and the independent variable is continuous. Before applying the Kruskal-Wallis test, the normality of the data was tested with the Shapiro-Wilk test, the data was checked for outliers using the quartile method and the homogeneity of variance was tested using Levene's test.

RESULTS AND DISCUSSIONS

The mechanical properties of the cylindrical specimens made from the materials used for manufacturing the abutments and crowns and tested under the load were evaluated initially. In Fig. 2 are shown the stress-strain curves of the investigated materials used to manufacture the abutments and crowns. Their mechanical behavior is essential in understanding the results obtained when two different materials are combined.

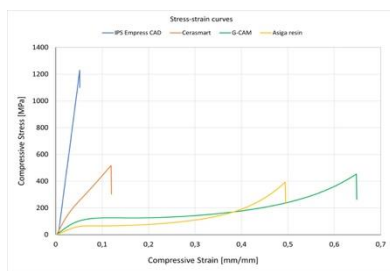


Figure 2. Stress-strain curves of the investigated materials

In order to evaluate the mechanical properties of the materials used for manufacturing the abutments and crowns, the stress-strain curves of the investigated materials were plotted. The stress-strain curves of the investigated materials are presented in Figure 2. In case of the molar crowns' samples, the descriptive statistics (average and standard deviation) regarding the maximum

compressive load and compressive

extension at maximum load for each material and thickness group are presented in

Table 2.

The distributions of values in each material category for the three thickness groups are depicted in Fig. 3 and Fig. c)

Figure 2.

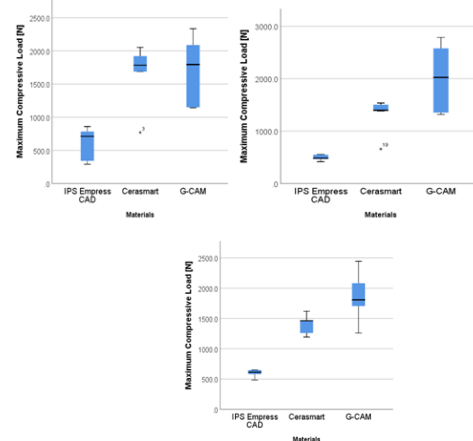


Figure 1. Distribution of maximum compressive load values of the three materials in: a) Group 1, b) Group 2, c) Group 3

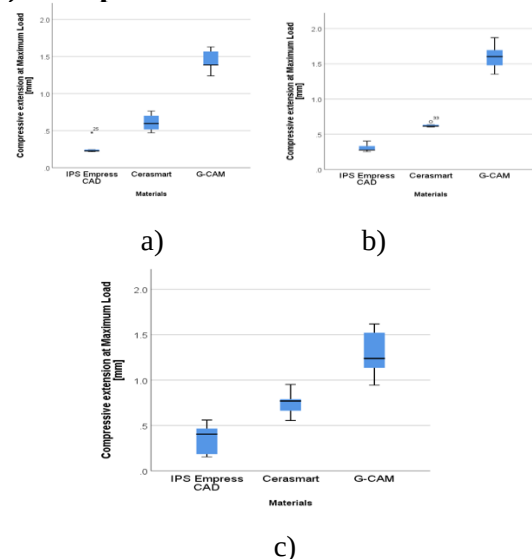


Figure 2. Compressive extension at

**maximum load for thickness groups:
a) Group 1, b) Group 2, c) Group 3**

The values for G-CAM samples show a much wider distribution than the values in the other two material groups. This applies to all measured characteristics.

The molar samples fabricated from IPS Empress CAD seem to have lower load values than both Cerasmart and G-CAM. To test if this difference is statistically significant, an analysis of variance was performed.

The following hypotheses can be formulated:

H1. There is no significant difference in maximum compressive load between materials in each thickness group.

H2. There is no significant difference in compressive extension at maximum load between materials in each thickness group.

H3. There is no significant difference in maximum compressive load between materials regardless of thickness group.

H4. There is no significant difference in compressive extension at maximum load between materials regardless of thickness group.

As the variables are continuous and there are three material groups, an ANOVA would be appropriate. The ANOVA requires that the data be approximately normally distributed,

there shouldn't be any significant outliers, and there should be homogeneity of variance. The Shapiro-Wilk test was used to determine if the data is approximately normally distributed (

Table 3).

The homogeneity of variance was tested using Levene's test of homogeneity of variance (Table 4). Most values show heterogeneity of variance.

Given the small sample size and the violation of some of the assumptions necessary for an ANOVA, the Kruskal-Wallis non-parametric test was used. It is the non-parametric alternative of ANOVA, does not have any assumption on the distribution of data and is more robust to outliers.

H1. The same type of test was used to determine if there is a significant difference in maximum compressive load between materials in different thickness groups. A significant difference between materials was found for all material thickness groups: 0.6-0.4 (H(2)=8.180, p=.017), 1-0.7 (H(2)=9.780, p=.008) and 1.5-1 (H(2)=11.180, p=.004). The distributions of the data were similar as observed from the box plot. A Dunn post-hoc test with a

Bonferroni correction revealed that in all cases G-CAM ($Me_{0.6-0.4}=1793.9N$, $Me_{1-0.7}=2024.85N$, $Me_{1.5-1}=1807.39N$) had a significantly higher maximum compressive load than Empress ($Me_{0.6-0.4}=711.8N$, $Me_{1-0.7}=483.2N$, $Me_{1.5-1}=613.9N$) (Table 5).

H2. The difference in compressive extension between materials in different thickness groups was also tested using the Kruskal-Wallis test. A significant difference between materials was found for all material thickness groups: 0.6-0.4 ($H(2)=11.520$, $p=.003$), 1-0.7 ($H(2)=12.020$, $p=.002$) and 1.5-1 ($H(2)=12.500$, $p=.002$). The distributions of the data were similar as observed from the box plot. A Dunn post-hoc test with a Bonferroni correction revealed that in all cases G-CAM ($Me_{0.6-0.4}=1.238mm$, $Me_{1-0.7}=1.386mm$, $Me_{1.5-1}=1.601mm$) had a significantly higher compressive extension than IPS Empress CAD ($Me_{0.6-0.4}=0.405mm$, $Me_{1-0.7}=0.226mm$, $Me_{1.5-1}=0.277mm$) (Table 5). Table 5 shows the test statistics for the Kruskal-Wallis tests with their corresponding adjusted p-values for each thickness group for the tested hypotheses.

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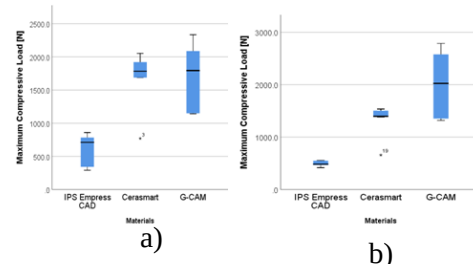
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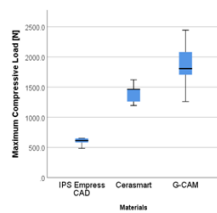
H3. The maximum compressive load was also significantly different between material groups ($H(2)=29.839$, $p<.001$). The distributions of the data were similar as observed from the box plot. A Dunn post-hoc test with a Bonferroni correction revealed that G-CAM ($Me=1807.4N$) and Cerasmart ($Me=1464.1N$) had a significantly higher maximum compressive load than IPS Empress CAD ($Me=555.5N$) ($Z_{G-CAM-IPSEmpressCAD}=3.920$, $p<.001$; $Z_{Cerasmart-IPSEmpressCAD}=-5.255$, $p<.001$).

H4. A significant difference between material groups was found also for the compressive extension at maximum values ($H(2)=38.271$, $p<.001$). The distributions of the data were similar as observed from the box plot. A Dunn post-hoc test with a Bonferroni correction revealed that G-CAM ($Me=1.478mm$) had a significantly higher compressive extension than both Cerasmart ($Me=0.635mm$) and IPS Empress CAD ($Me=0.273mm$) ($Z_{G-CAM-Empress}=-3.156$, $p=.005$; $Z_{G-CAM-Cerasmart}=-6.186$, $p<.001$, $Z_{Cerasmart-IPSEmpressCAD}=3.030$, $p=.007$).

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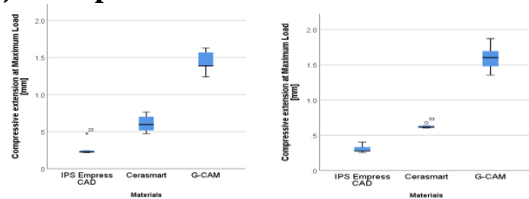
Figure 2.





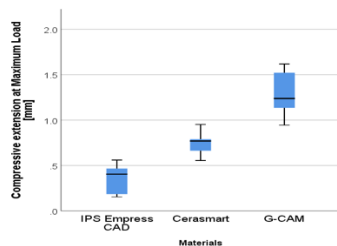
c)

Figure 1. Distribution of maximum compressive load values of the three materials in: a) Group 1, b) Group 2, c) Group 3



a)

b)



c)

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Table 1. Descriptive statistics of the cylindrical specimens

Material	Compressive Stress [MPa]		Compressive Strain [mm/mm]		Young's Modulus [MPa]	
	Average	Std. Dev.	Average	Std. Dev.	Average	Std. Dev.
IPS						
Empress	1257.8	69.46	0.04974	0.00205	27540.7	295.77
CAD						
Cerasmart	501.3	35.51	0.11526	0.00955	6358.9	159.96
G-CAM	435.3	33.53	0.64993	0.00222	2598.7	12.02
Asiga resin	360.4	28.25	0.51604	0.03082	1458.4	84.54

Table 2. Descriptive statistic of the test results for molar crowns samples

Material	Thickness	Maximum Compressive load [N]		Compressive extension at Maximum load [mm]	
		Average	Std. Dev.	Average	Std. Dev.
IPS	0.6-0.4	597.5	262.1	0.354	0.177
Empress	1-0.7	494.3	68.4	0.276	0.061
CAD	1.5-1	596.1	68.4	0.308	0.061
Cerasmart	0.6-0.4	1642.9	507.7	0.746	0.148
	1-0.7	1295.4	362.4	0.610	0.123
	1.5-1	1400.7	172.4	0.629	0.030
G-CAM	0.6-0.4	1701.5	542.1	1.291	0.277
	1-0.7	2011.8	677.5	1.441	0.157
	1.5-1	1860.1	440.5	1.599	0.199

Table 3. The Shapiro-Wilk test of normality

Characteristic	Thickness	IPS Empress CAD			Cerasmart			G-CAM		
		Statistic	df	Sig.	Statistic	df	Sig.	Statistic	df	Sig.
Maximum Compressive load	0.6-0.4	0.851	5	0.198	0.803	5	0.086	0.883	5	0.323
	1-0.7	0.919	5	0.526	0.714	5	0.013	0.88	5	0.311
	1.5-1	0.85	5	0.195	0.932	5	0.61	0.992	5	0.985
Compressive extension at Maximum load	0.6-0.4	0.903	5	0.427	0.982	5	0.946	0.952	5	0.754
	1-0.7	0.641	5	0.002	0.95	5	0.736	0.937	5	0.645
	1.5-1	0.871	5	0.269	0.834	5	0.15	0.994	5	0.991

Table 4. The Levene's test of homogeneity

Characteristics	Thickness	Levene Statistic	df1	df2	Sig.
Maximum Compressive Load	0.6-0.4	1.157	2	12	0.347
	1-0.7	6.448	2	12	0.013
	1.5-1	4.061	2	12	0.045
Compressive extension at Maximum Load	0.6-0.4	1.902	2	12	0.192
	1-0.7	0.687	2	12	0.522
	1.5-1	4.861	2	12	0.028

Table 5. Test statistic with adjusted significance for groups G-CAM and IPS Empress CAD

Thickness	Maximum Compressive load [N]		Compressive extension at Maximum load [mm]	
	z	Adj. Sig.	z	Adj. Sig.
0.6-0.4	-2.687	0.022	-3.394	0.002
1-0.7	-2.970	0.009	-3.465	0.002
1.5-1	-3.323	0.003	-3.536	0.001

The experimental study aimed to investigate the mechanical behavior of three CAD/CAM restorative materials: IPS Empress CAD (Ivoclar Vivadent), Cerasmart (GC) and G-CAM (Grafenano Dental) used for the fabrication of the molar crowns and tested in terms of the resistance to axial compressive load. The samples formed from cemented crowns on the Asiga resin dies and the cylindrical specimens fabricated from each type of material were analyzed and the correlations between the mechanical properties of the crowns and abutments' materials were also made to simulate *in vitro* the action of occlusal forces during the mastication process on the complete crowns in the posterior teeth.

The results suggested that the mean values of maximum compressive load for G-CAM crowns were statistically significantly higher than those of IPS Empress CAD and Cerasmart for the same thickness group. The statistically significant differences regarding the compressive load were found between G-CAM and IPS Empress CAD crowns.

Between G-CAM and Cerasmart materials there are differences in this regard, but not statistically significant. It can be stated that the null hypothesis has been rejected in both circumstances after assembling and assessing the data.

The physiological and normal mastication force varies from 70 to 150N, with a maximal biting force of 500 to 700N, according to Scully's Oxford Handbook of Dental Science [28]. Several other studies have corroborated this, despite the fact that maximal biting forces of up to 1000N have been documented in the past among some Eskimo groups [29-32].

The mechanical properties of restorative materials have impact on the clinical performance and long-term longevity of CAD/CAM restorations. These properties differ from one type of material to another and mainly depend on the microstructure [2,20].

The compressive strength and Young's modulus are the important properties of the materials to be considered when assessing the mechanical behavior of

crown materials and abutment substrates by reason of the chewing forces. The values of the compressive strength and Young's modulus for the tested materials were for IPS Empress CAD 1258 MPa and 27 GPa; for Cerasmart 501.3 MPa and 6.3 GPa and for G-CAM 435 MPa and 2.5 GPa. Based on the results of this experimental study, the compressive strength and Young's modulus for the Asiga resin material were 360 MPa and 1.4 GPa, in comparison with the dentin as the tooth substrate values the compressive strength is 297 MPa and modulus of elasticity for compression is 17 GPa [33,34]. These findings indicated the difference between modulus of elasticity of the Asiga resin used as the abutment material and the dentin.

Combining materials with different toughness will influence the mechanical behavior of CAD/CAM manufactured molar samples. The abutment has a more ductile behavior with large deformations until fracture and the crowns made of a brittle material will fracture at lower compressive forces with a glass-like fracture pattern. Due to the fragile behavior, the analyzed thickness of the IPS Empress CAD crowns does not have a significant influence on the compressive strength of the samples; almost all the samples presented the defects at the crowns, only in the form of chips. Our results showed that IPS Empress CAD has significantly lower force bearing values than the other two materials (Cerasmart and G-CAM), in spite of the fact that leucite-based ceramics have a crystalline phase that enhances the mechanical properties of the material, with quantity and homogeneity of the crystals being the essential factors preventing the crack propagation [35].

Fradeani *et al.* clinically assessed 125 crowns made of leucite-reinforced glass ceramic over 11-year period, showing a high survival probability of 95.2% (98.9% for anterior teeth and 84.4% for posterior teeth). The authors concluded that these crowns exhibited low failure rate, excellent aesthetic and emphasized the importance of using adhesive cementation technique for ensuring the success rate [36].

A study carried out by Murgueitio analysed the survival rate and failure mode of IPS leucite-reinforced ceramic onlays and partial crowns by measuring occlusal thickness and performing a 3-year follow-up and demonstrated that increased material thickness determines a lower chance of failure, and vital teeth are less likely to fail compared to non-vital ones [37].

A controlled clinical trial conducted by Frankenberger assessing 96 IPS Empress indirect restorations (inlays and onlays) over a 12-year period found satisfactory clinical results, with a low failure rate of 16% and with more bulk fractures when cementation was performed with a light-curing composite. The restorations with dual cure resin cement exhibited significantly fewer bulk fractures [38].

An *in-vitro* study conducted by Heintze evaluated mandibular molar crowns made of IPS Empress and IPS e.max Press adhesively cemented on CAD/CAM milled PMMA abutments during static and dynamic loading. All crowns were loaded by applying an eccentric force in a chewing simulator. Another four crowns of each material were subjected to force measurements with a 3D force sensor during dynamic loading using two different lateral movements (from fossa to cusp and vice versa). The fracture

rate of IPS Empress molar crowns was higher compared to IPS e.max Press, 50% of the IPS Empress crowns failed (75% fractures and 25% chippings) during dynamic loading, while lithium disilicate ceramic molar crowns presented no fracture, even if the forces exerted on the crowns and abutments were 2-3 times higher than those during static loading [18].

In our study, molar samples manufactured with Cerasmart crowns proved to have a higher load resistance compared to IPS Empress CAD crowns but a slightly lower one than G-CAM. The results can be explained by the fact that Cerasmart and Asiga resin have similar ultimate stress, but the crown material will be more brittle. In Group 1, the samples have more complete fractures because the low thickness of the crown contributes to a lesser extent to the overall strength of the sample. As the crown thickness increases, the number of complete fractures decreases, the material contributing more to the strength of the sample; increased thickness leads to a higher strength of molar samples. The results of this study are confirmed by other studies, which demonstrated a high compressive strength and good fracture performance for resin ceramic materials [18].

Jassim *et al.* performed a comparative assessment of fracture strength for crowns made of CAD/CAM materials (lithium disilicate, zirconia, reinforced composite, hybrid ceramic - Cerasmart and zirconia-reinforced lithium silicate) on first premolars prepared teeth, extracted for orthodontic purposes, which were subjected, post cementation, to an axial compressive force, and noticed the differences between these materials with regard to fracture strength owing to their

different chemical composition and microstructure [39].

A clinical study evaluated for a period from 1 to 9 years the clinical performance of 121 all ceramic crowns, fabricated by IPS Empress 2 system, placed on the vital teeth, except for 11 crowns fixed on endodontically treated teeth. It was found a survival rate of 95.24% after 5 years and 87.1% up to 9 years and all ceramic crowns applied on the endodontically treated teeth without post and core restorations showed a higher failure rate compared to all-ceramic crowns on vital teeth [40].

Mechanical compatibility in terms of maximum compressive stresses and strains between the material of abutments (Asiga resin) and crowns made of G-CAM will lead to higher compressive loads that can be applied onto the molar samples. For G-CAM, as the thickness of the crowns increases and the material have the same properties, the samples presented complete fracture (abutment and crown). The thicker the crowns in Group 3, the more the numbers of complete fractures (abutment and crown) increase. At present, there are relatively few studies focusing on the G-CAM material, which is why it was not possible to correlate the results of the present study with others.

There are several limitations of this study: the small sample size - a larger sample would be needed to account for the great variability between samples, the testing conditions do not reflect the complexity of the oral cavity and used a simplified model that considers only the axial compressive load on the dental crown and 3D resin printed abutment as a substrate, obtained in the standardized way. Further studies are required to evaluate the

CAD/CAM materials in similar conditions to those in the oral environment and to reproduce the action of the chewing forces. The aspects investigated in this study could

be taken into consideration when clinicians choose the appropriate material for the prosthetic rehabilitation in various clinical situations.

CONCLUSIONS

1. IPS Empress CAD and Cerasmart materials have a fragile behavior, with a high compressive strength and Young's modulus compared to G-CAM and Asiga resins.
2. The mechanical behaviour of the individual materials influences the values of the compressive strength on the molar samples. By combining materials with different toughness levels, it can be stated that the abutments have a more ductile behavior, with large deformations under compressive load, whereas Cerasmart crowns present higher load resistance compared to IPS Empress CAD crowns, but slightly lower than G-CAM.

3. The mechanical compatibility between abutments and G-CAM crowns regarding the maximum compressive stresses and strains enables higher compressive loads to be applied on the molar samples.

4. For IPS Empress CAD, crown thickness does not have a significant influence on compressive strength. For Cerasmart, the thickness increases as the number of complete fractures decreases. For G-CAM, if the thickness increases and the materials have the same properties, the number of complete fractures increases also.

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